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***RobLib*: A Library of Models for Industrial Robots**

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Abstract

This paper describes a software package developed in the Windows environment. This software consists of a library for industrial robots models and allows the calculation of the direct and the inverse kinematics for several manipulators. The program allows trajectory planning algorithms, both in the joint and cartesian spaces, using linear or cubic splines interpolation procedures. The kinematic equations for each robot were optimised in what concerns the number of required operations in order to optimize the computational load.

Key Words: Robots, Kinematics, Trajectory Planning, Software.

1. Introduction

This paper introduces the *RobLib* package and describes his functional aspects. Given the popularity of Microsoft Windows it was decided to implement the software in this environment using the Microsoft Visual Basic language.

Many programs are available for modelling robots but most of them focus on simulation aspects [1,9]. *RobLib* consists in a library of models and algorithms for standard industrial manipulators. It contains several robots with different mechanical structures and up to six joints (rotational and prismatic). For each robot the user can calculate the direct and inverse kinematics for the positions, the velocities and the accelerations using Homogeneous Transformation Matrices (HTMs), Euler Parameters or Euler Angles. The trajectory planning algorithms can be executed using linear or cubic splines interpolation procedures, either in the operational or in the joint spaces.

In this line of thought, the paper is organised as follows. Section 2 gives an overview of the software capabilities including some application examples. Based on this description, section 3 draws the main conclusions and presents the perspectives towards future software enhancements.

2. Overview of the Software

The *RobLib* package was designed to take full advantage of the Windows environment. All the commands and data are entered through pull down menus, buttons and dialog boxes. The program has a modular structure; therefore, improvements and modifications can be made without affecting the other modules. Moreover, new modules can be easily added to expand the software package.

The main window contains a menu bar that includes the following entries: File, Robot and Help.

The Robot menu (Fig. 1a) allows the user to choose the robot to be studied. The robot is classified by the series of joints from the base to the hand (e.g. Portique 80 - PPPRRR). After selecting a robot, *RobLib* presents a new window (fig. 1b) whose menu has two major choices: Kinematics and Trajectory Planning that are described in the next two sub-sections.

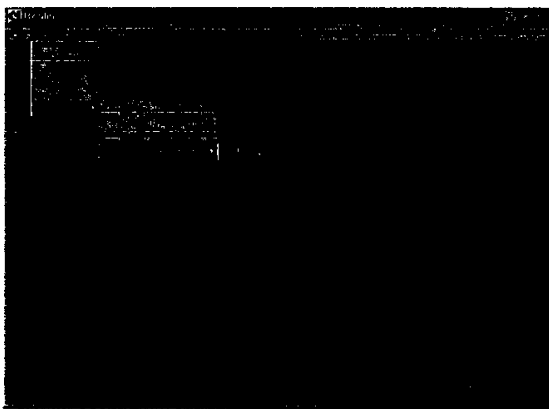


Fig. 1a - *RobLib* main window

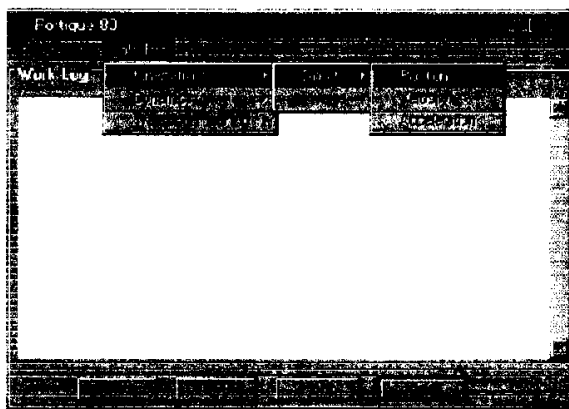


Fig. 1b - Window for the Portique 80 robot.

2.1. Kinematics

The direct kinematics consists on determining the position and orientation of the end-effector in the cartesian space given the values of the robot joint variables. The mathematical foundations are the concept of HTMs and the Denavit-Hartenberg (DH) formalism [10-16] of assigning coordinate frames at each robot joint. *RobLib* provides information about the DH parameters for each robot as well as a schematic representation of the mechanical structure.

The results of the direct kinematics can be seen in HTM (representing the end-effector coordinates in the base reference frame) or, alternatively, using cartesian coordinates for the position and Euler Parameters or Euler Angles for the orientation [17].

Using a rectangular coordinate system for the end-effector (Fig. 2), consisting of the unit vectors \mathbf{n} , \mathbf{s} , \mathbf{a} , can be defined a 4x4 HTM $\mathbf{T}_{1,n+1}$ as in (1), in which \mathbf{p} indicates the gripper position relatively to the base.

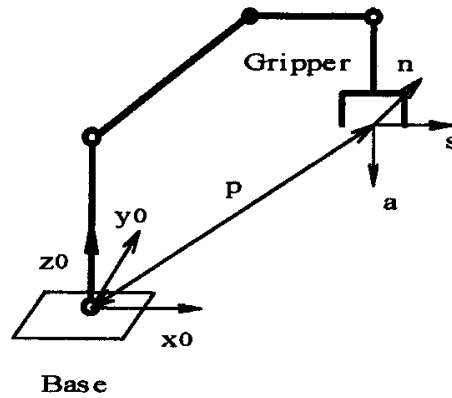


Fig. 2 - Local end-effector coordinate frame.

$$\mathbf{T} = \begin{bmatrix} \mathbf{n} & \mathbf{s} & \mathbf{a} & \mathbf{p} \\ 0 & 0 & 0 & 1 \end{bmatrix} = \begin{bmatrix} n_x & s_x & a_x & p_x \\ n_y & s_y & a_y & p_y \\ n_z & s_z & a_z & p_z \\ \hline 0 & 0 & 0 & 1 \end{bmatrix} \quad (1)$$

Moreover, the Euler parameters can be expressed in terms of the vectors \mathbf{n} , \mathbf{s} and \mathbf{a} as:

$$\begin{aligned} p_E &= \frac{1}{2} \operatorname{sgn}[s_z - a_y] \sqrt{n_x - s_y - a_z + 1} \\ q_E &= \frac{1}{2} \operatorname{sgn}[a_x - n_z] \sqrt{s_y - a_z - n_x + 1} \\ r_E &= \frac{1}{2} \operatorname{sgn}[n_y - s_x] \sqrt{a_z - n_x - s_y + 1} \\ s_E &= \sqrt{1 - p_E^2 - q_E^2 - r_E^2} \end{aligned} \quad (2)$$

Fig. 3 depicts the results of the direct kinematics, in Euler Parameters, for the Portique 80 robot and a given set of inputs. The joint limits specify the range of variation for each joint. For a revolute/prismatic joint the limits are specified as the minimum and maximum angles/extensions. Those limits can not be exceeded and a warning message appears if the user tries to enter improper values.

Identical procedures are available for the velocities and accelerations. The calculation of the joint velocities requires the previous calculation of the joint positions. Furthermore, the calculation of the accelerations implies the previous calculation of the joint positions and velocities. Therefore, those options activated, consecutively, during the program session.

The inverse kinematics may lead to more than one solution [10-12]. For a given configuration the inverse kinematics implies the determination of the required joint variables. In fact, many robots exhibit multiple solutions representing different sets of joint displacements that yield the same gripper configuration (Fig. 4). The analytical solution for inverse position is obtained either through the decoupling of the kinematic equations [17] or using the trigonometric method [12].

Position Direct Kinematics	Velocity Direct Kinematics	Acceleration Direct Kinematics
<p>Sub DKPM_PORTIQUE80 ()</p> <p>C4 = OPTCOS(Q(4)) C5 = OPTCOS(Q(5)) C6 = OPTCOS(Q(6)) S4 = OPTSIN(Q(4)) S5 = OPTSIN(Q(5)) S6 = OPTSIN(Q(6))</p> <p>R6 = PORTmat(7, 5)</p> <p>'Portique80 DKPM Equations</p> <p>D01 = S5 * R6 D02 = S4 * D01 D03 = C4 * D01 D04 = C5 * R6 D05 = S5 + C6 D06 = C4 * D05 D07 = S5 - S4 D08 = S6 * D07 D09 = C6 + S4 D10 = S5 * D09 D11 = S4 - C6 D12 = S5 * D11 D13 = S4 * C6 D14 = C4 * C5 D15 = D14 * S6 D16 = S5 * D09 D17 = S4 * C5 * S6 D18 = D14 * C6 D19 = D13 + 1 D20 = D19 - D15 D21 = C4 * S6 D22 = C5 * (1 - D13)</p> <p>'RESULTS</p> <p>L = Q3 - D04 M = Q2 - D02 N = Q1 + D03 PE = .5 * Sgn(D06 + D17) * Sqr(D20 + D16) QE = .5 * Sgn(D08 - D18) * Sqr(D20 - D16) RE = .5 * Sgn(D21 + D22) * Sqr(D15 - D13 + D12 + 1)</p> <p>End Sub</p>	<p>Sub DKVM_PORTIQUE80 ()</p> <p>C4 = OPTCOS(Q(4)) C5 = OPTCOS(Q(5)) S4 = OPTSIN(Q(4)) S5 = OPTSIN(Q(5))</p> <p>d26 = PE * PE d27 = QE * QE d28 = RE * RE d29 = d26 + d27 + d28 SE = Sqr(1 - d26 - d27 - d28)</p> <p>R6 = PORTmat(7, 5)</p> <p>D01 = R6 * DQ5 D02 = S5 * D01 D03 = R6 * DQ4 D04 = S5 * D03 D05 = C5 * D01 D06 = S4 * D05 D07 = C4 * D05 D08 = C4 * D04 D09 = S4 * D04 D10 = SE * DQ4 D11 = RE * DQ4 D12 = QE * DQ4 D13 = C4 * SE + S4 * PE D14 = S4 * SE - C4 * PE D15 = RE * C4 - S4 * QE D16 = S4 * RE + C4 * QE D17 = S5 * D16 + C5 * SE D18 = S5 * D14 D19 = C5 * RE - D18 D20 = D13 * S5 D21 = D20 - C5 * QE D22 = S5 * DQ6</p> <p>'RESULTS</p> <p>DL = D02 + DQ3 DM = -DQ2 - D08 - D06 DN = DQ1 - D09 + D07 DPE = .5 * (D10 + D15 * DQ5 - D17 * DQ6) DQE = .5 * (D13 * DQ5 - D11 + D19 * DQ6) DRE = .5 * (D12 + D14 * DQ5 + D21 * DQ6)</p> <p>End Sub</p>	<p>Sub DKAM_PORTIQUE80 ()</p> <p>C4 = OPTCOS(Q(4)) C5 = OPTCOS(Q(5)) S4 = OPTSIN(Q(4)) S5 = OPTSIN(Q(5))</p> <p>E1 = PE * PE E2 = QE * QE E3 = RE * RE E4 = E1 + E2 + E3</p> <p>SE = Sqr(1 - E1 - E2 - E3) DSE = -(PE * DPE + QE * DQE + RE * DRE) / SE R6 = PORTmat(7, 5)</p> <p>D01 = S5 * R6 D02 = C5 * R6 D03 = DQ5 * DQ5 D04 = DQ4 * DQ4 D05 = D04 * DQ5 D06 = D03 * DQ4 D07 = C4 * DQ2 D08 = S4 * DQ2 D09 = C4 * DQ1 D10 = S4 * DQ1 D11 = RE * C4 - S4 * QE D12 = RE * S4 + QE * C4 D13 = DRE * C4 - DQE * S4 D14 = DRE * S4 + DQE * C4 D15 = DQ4 * DQ5 D16 = DQ4 * DQ6 D17 = DQ5 * DQ6 D18 = SE * C4 + PE * S4 D19 = PE * C4 D20 = SE * S4 D21 = D19 - D20 D22 = DSE * C4 + DPE * S4 D23 = DPE * C4 - DSE * S4 D24 = PE * C4 + SE * S4 D25 = DSE * S4 - DPE * C4 D26 = DPE * S4 + DSE * C4</p> <p>'RESULTS</p> <p>DDL = DDQ3 + D01 * DDQ5 + D02 * D03 DDM = -DDQ2 - D09 * DDQ4 - D08 * DDQ5 + D08 * D05 + D09 * D06 DDN = DDQ1 - D10 * DDQ4 + D07 * (DDQ5 - D05) + D10 * D06 DDPE = .5 * (SE * DDQ4 + D11 * DDQ5 - (S5 * D12 + C5 * SE) * DDQ6 + DSE * DQ4 + D13 * DQ5 - D12 * D15 - (S5 * D14 + C5 * DSE) * DQ6 - S5 * D11 * D16 - (C5 * D12 - S5 * SE) * D17) DDQE = .5 * (D18 * DDQ5 - RE * DDQ4 + (S5 * D21 + C5 * RE) * DDQ6 - DRE * DQ4 + D22 * DQ5 + D21 * D15 + (C5 * DRE + S5 * D21) * DQ6 - S5 * D18 * D16 + (C5 * D21 - S5 * RE) * D17) DDRE = .5 * (QE * DDQ4 - D19 * DDQ5 + (S5 * D24 - C5 * QE) * DDQ6 + DQE * DQ4 + D25 * DQ5 + D24 * D15 + (S5 * D26 - C5 * DQE) * DQ6 + S5 * D19 * D16 + (C5 * D24 + S5 * QE) * D17)</p> <p>End Sub</p>

Table 1- Optimized equations of the direct kinematics (using Euler Parameters) of the robot Portique80

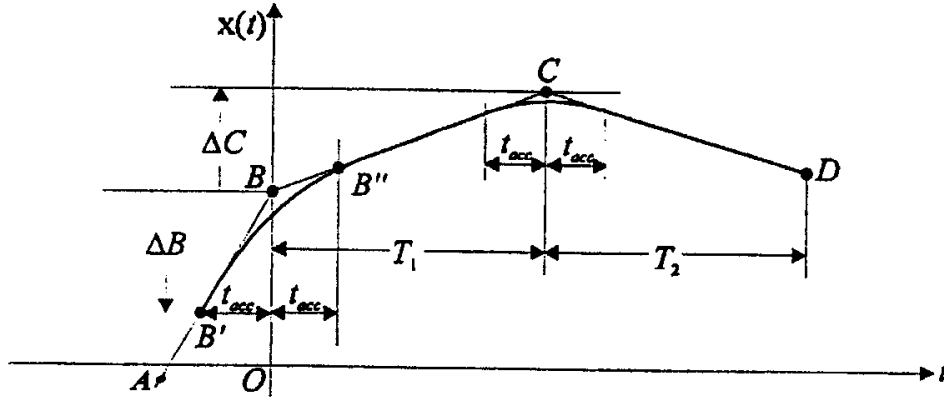


Fig. 5 – Transition between two adjacent straight line segments

If the user chooses straight lines, he can define the acceleration time allowed at the trajectory corner points, that is, he can establish the motion softness at these points.

A straight line trajectory between two points can be described by equation (3) where $p(t) \in [0,1]$ allows the choice of a velocity profile.

$$x(t) = x_0 + p(t) (x_f - x_0), \quad 0 \leq t \leq T \quad (3)$$

Often, there are not just two but a set of several points through which the end-effector must pass. In order to achieve a smooth motion, and avoid velocities discontinuities, the desired trajectory must be planned so that the straight lines are “bented” around the corner points that join two adjacent line segments (Fig 5). Therefore, in the interval $-t_{acc} \leq t \leq t_{acc}$ the trajectory is given by equations (4-8) for the position, velocity and acceleration.

$$x(t) = \left[\left(\Delta C \frac{t_{acc}}{T_1} + \Delta B \right) (2-h)h^2 - 2\Delta B \right] h + B + \Delta B \quad (4)$$

$$\dot{x}(t) = \left[\left(\Delta C \frac{t_{acc}}{T_1} + \Delta B \right) (1.5-h)2h^2 - \Delta B \right] \frac{1}{t_{acc}} \quad (5)$$

$$\ddot{x}(t) = \left(\Delta C \frac{t_{acc}}{T_1} + \Delta B \right) (1-h) \frac{3h}{t_{acc}^2} \quad (6)$$

$$h = \frac{t + t_{acc}}{2t_{acc}}, \quad -t_{acc} \leq t \leq t_{acc} \quad (7)$$

$$\Delta C = C - B \quad ; \quad \Delta B = B' - B \quad (8)$$

The bending of the desired trajectory is followed by a straight line with constant velocity according with the equations:

$$\mathbf{x}(t) = \Delta C \mathbf{h} + \mathbf{B} ; \mathbf{h} = \frac{t}{T_1} \quad (9)$$

$$\dot{\mathbf{x}}(t) = \frac{\Delta C}{T_1} \quad (10)$$

$$\ddot{\mathbf{x}}(t) = 0 \quad (11)$$

Based on these equations, *RobLib* calculates the corresponding joint variables. For example, Fig. 6 shows the time evolution of positions, velocities and accelerations, given six points defined in joint space, using linear interpolation with $t_{acc} = 2$ seconds for the Portique 80 robot. The algorithm assures the velocity and the acceleration continuity at all points, including the initial and the final locations, by introducing two extra points in the trajectory.

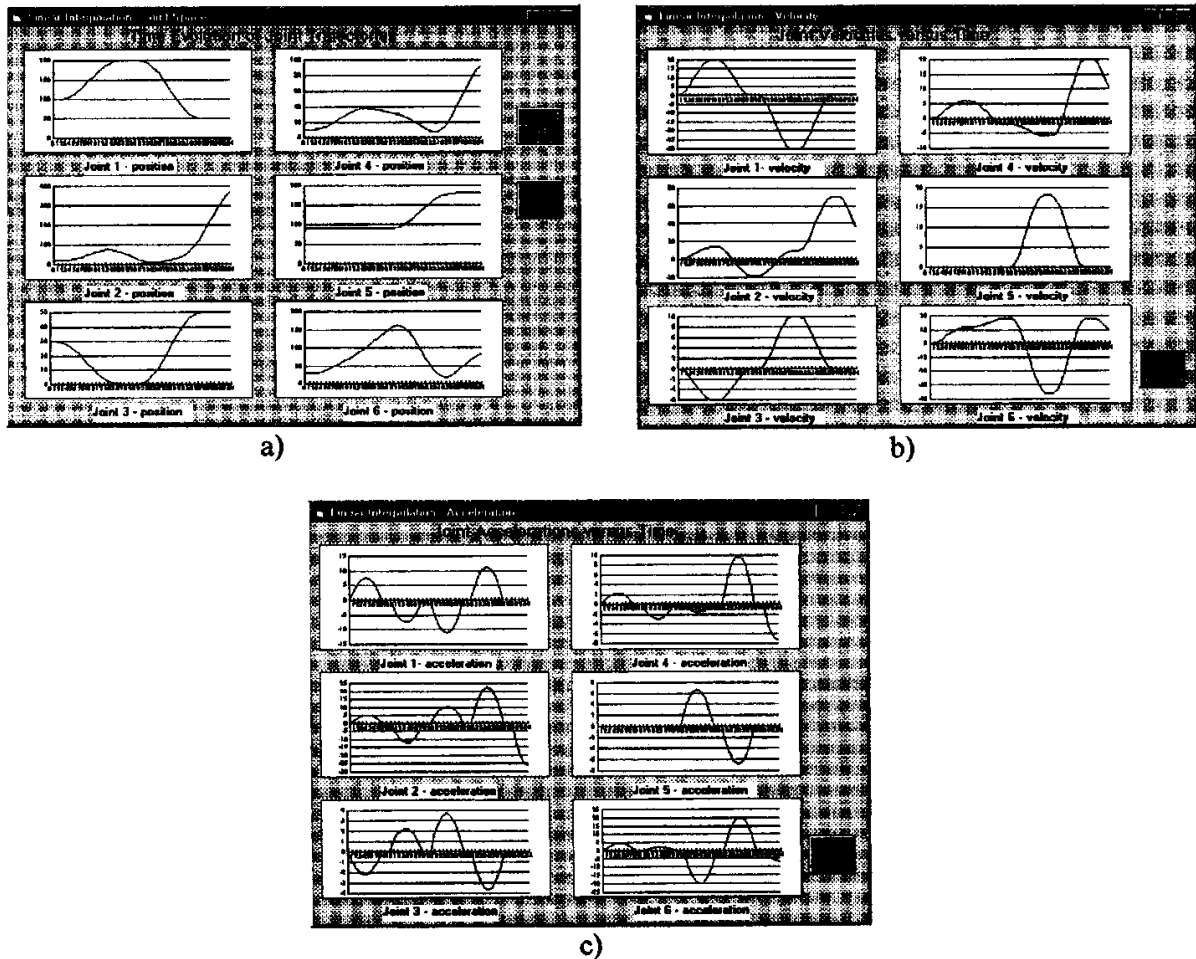


Fig. 6 - Time evolution of joint variables using a linear interpolation in the joint space with $t_{acc} = 2$ seconds.

- a) Positions,
- b) Velocities,
- c) Accelerations.

3. Conclusions and Future Developments

A program for the calculation of the direct and the inverse kinematics and trajectory planning algorithms was presented. The *RobLib* program is implemented in Visual Basic for Microsoft Windows and provides a library of models for industrial robots.

Future versions will expand the capabilities of *RobLib* in order to include new trajectory planning interpolation procedures and to implement dynamic and control algorithms. Due to *RobLib* modular structure improvements and modifications can be made without affecting the rest of the program and, therefore, new modules can be easily added to expand the package.

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