

# Determination of total petroleum hydrocarbons in soil from different locations using infrared spectrophotometry and gas chromatography

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## ABSTRACT

Total petroleum hydrocarbons (TPH) are important environmental contaminants which are toxic to human and environmental receptors. Several analytical methods have been used to quantify TPH levels in contaminated soils, specifically through infrared spectrometry (IR) and gas chromatography (GC). Despite being two of the most used techniques, some issues remain that have been inadequately studied: a) applicability of both techniques to soils contaminated with two distinct types of fuel (petrol and diesel), b) influence of the soil natural organic matter content on the results achieved by various analytical methods, and c) evaluation of the performance of both techniques in analyses of soils with different levels of contamination (presumably non-contaminated and potentially contaminated). The main objectives of this work were to answer these questions and to provide more complete information about the potentials and limitations of GC and IR techniques. The results led us to the following conclusions: a) IR analysis of soils contaminated with petrol is not suitable due to volatilisation losses, b) there is a significant influence of organic matter in IR analysis, and c) both techniques demonstrated the capacity to accurately quantify TPH in soils, irrespective of their contamination levels.

## Keywords

Total petroleum hydrocarbons, soil, infrared spectrophotometry, gas chromatography

## Introduction

Soils contaminated with petroleum products create widespread environmental problems due to their adverse effects (Wang et al., 1999). It is becoming urgent to assess contamination in some sites in question, to remediate and monitor these cleaning processes and to evaluate final quality of the soil.

TPH are an important group of environmental contaminants that are toxic to human and environmental receptors (Park & Park, 2011). In 1999 the United States Environmental Protection Agency (USEPA) Site Program began its evaluation of field methods for the determination of TPH in soils. This was an ambitious project that involved the establishment of a TPH definition and the development of a reference

method for its quantification. One of the methods selected for this evaluation was SW-846 Method 9074 (Lynn et al., 2002; USEPA, 1996a).

At present, a wide variety of specific and non-specific methods are used for analysis of TPH. The conventional non-specific methods include: i) field-screening gas chromatography with flame ionisation (GC-FID) or photo-ionisation detection (GC-PID) (API, 1992, 1994; USEPA, 1996b), ii) gravimetric determination and infrared spectrophotometry (IR), such as USEPA methods 418.1, 8440, and 9071B, and American Society for Testing and Materials (ASTM) methods 3414 and 3921 (USEPA, 1978, 1996c, 1998; ASTM, 1997a, 1997b), iii) turbidimetry (USEPA, 1996a), iv) ultraviolet and fluorescence spectroscopy (Burns, 1993; ASTM 1997c), v) thin-layer chromatog-

raphy (TLC) (which has been extensively used in the component class characterisation of various oils and respective fractions) (Wang et al., 2010), vi) high performance liquid chromatography (HPLC) (Krahn et al., 1993), vii) size-exclusion chromatography (Krahn & Stein, 1998), viii) supercritical fluid chromatography (SFC) (ASTM, 1997d), ix) total organic carbon (Schreier et al., 1999), x) isotope ratio mass spectrometry (Wang et al., 1999), and xi) fibre optic IR sensor for identification of various petroleum samples (Ge et al., 1995). The non-specific techniques have been used to screen TPH and petroleum saturated and aromatic compounds in sediments, to assess site contamination, to identify and quantify petroleum products that may exist in soil or water, and to qualitatively analyse and compare oil degradation due to weathering (Wang et al., 1999).

Fingerprint analysis has been developed using specific and advanced techniques such as: i) gas chromatography–mass spectrometry (GC-MS), ii) high performance liquid chromatography–mass spectrometry (HPLC-MS), iii) isotope dilution mass spectrometry (IDMS), iv) nuclear magnetic resonance (NMR), and v) electrospray ionisation–mass spectrometry (ESI-MS) (Wang & Fingas, 1997, 2003; Eide & Zahlsen, 2005; Daling et al., 2002). Many USEPA and ASTM methods have been modified to improve selectivity and sensitivity for measuring spilled oil and petroleum products in soils and water (ASTM, 1997a, 1997b, 1997e, 1997f, 1997g; Sink & Hardy, 1994).

Wright (1995) reported that using field measurement methods instead of laboratory analyses it was possible to analyse more soil samples, faster and at lower cost. Lambert et al. (2001) used two test kits for soil analyses: the immunoassay-based EnviroGard and petroleum fuel in soil test kit and a colorimetric test procedure (DR/2000). Lynn et al. (2002) analysed performance of the PetroFLAG hydrocarbon analyser system (commercial version of SW-846 Method 90747). Using co-elution in a single-step chromatographic separation, it is impossible to identify and quantify the target compounds. Combined methods such as: HPLC-GC, GC-GC, GC×GC (two-dimensional GC), or supercritical fluid chromatography (SFC) are commonly used to improve the quality of analysis. Pál et al. (1998) used SFC-GC/MS for detailed analysis of different hydrocarbon groups in the range of petroleum fractions and Mao et al. (2009) estimated eco-toxicity of petroleum hydrocarbon mixtures in soil using HPLC-GC×GC. All these analytical methods have been modified in order to eliminate matrix interferences, reduce the amount of solvent used, find alternative and less toxic solvents, simplify analytical procedures amongst other requirements.

Methods of GC and IR techniques are commonly used to determine levels of TPH in contaminated soils; however, some issues remain that have not been sufficiently studied. These issues are studied in this work

and focus on: a) applicability of both techniques to the analysis of soils contaminated with two distinct types of fuel (petrol and diesel), b) influence of soil natural organic matter on TPH determination, and c) evaluation of the performance of both techniques on the analysis of soils with different levels of contamination (presumably non-contaminated and potentially contaminated). The work sought to provide a response to these questions and to supply more complete information on the potentials and limitations of GC and IR techniques applied to TPH determination.

## Experimental

### Materials and methods

The ASTM D5307 (ASTM, 1997h) Crude oil quantitative STD analytical standard was obtained from Supelco (Bellefonte, PA, USA), and diesel and petrol were acquired from a Portuguese oil refinery (Petrogal, S.A., Porto). Isooctane, pentane, potassium dichromate, and ortho-phosphoric acid of 85 mass % were obtained from Merck (Darmstadt, Germany), 1,1,2-trichloro-1,2,2-trifluoroethane and hexadecane were obtained from Sigma-Aldrich (Bellefonte, PA, USA). Sodium sulphate, ammonium iron(II) sulphate hexahydrate, and benzene were obtained from Riedel-de Haën (Seelze, Germany), and sulphuric acid 95–97 mass % was obtained from Fluka (Bellefonte, PA, USA). All reagents were of analytical grade or higher purity.

Deionised water ( $15.0 \text{ M}\Omega \text{ cm}^{-1}$ ) was produced using an Elix3 Advantage system (Millipore, Molsheim, France). High-purity grade silica gel (Davisil Grade 635), pore size: 60 Å, 60–100 mesh was purchased from Sigma-Aldrich (Bellefonte, PA, USA).

Following the EPA Method 8440 (USEPA, 1996c), the standard solution for IR was prepared by mixing hexadecane, isooctane, and benzene as the “reference oil” in a 50-mL glass-stoppered bottle. The integrity of the mixture was maintained by keeping the bottle duly stoppered except when withdrawing aliquots. The stock solution was prepared by diluting the reference oil 200-fold with 1,1,2-trichloro-1,2,2-trifluoroethane. A stock solution for GC determination was prepared by a 100-fold dilution of diesel with pentane. Working standards were prepared by accurate dilution of the stock solutions using 1,1,2-trichloro-1,2,2-trifluoroethane for IR and pentane for GC-FID on the day of use. All solutions were stored at 4 °C. The ASTM D5307 reference oil was prepared in 1,1,2-trichloro-1,2,2-trifluoroethane for IR determination and in pentane for GC analysis.

For determination of the organic matter content, three solutions were prepared: a)  $0.40 \text{ mol L}^{-1}$  ammonium iron(II) sulphate hexahydrate (SFA) in  $0.40 \text{ mol L}^{-1}$  sulphuric acid; ii) oxidant mixture of  $0.068 \text{ mol L}^{-1}$  potassium dichromate in  $7.50 \text{ mol L}^{-1}$  sul-

phuric acid and 3.85 mol L<sup>-1</sup> ortho-phosphoric acid, and iii) potassium dichromate 0.033 mol L<sup>-1</sup> in de-ionised water.

An IR Spectrolab Interspec 200X, Fourier transform infrared spectrometer (FTIR, Garforth, Leeds, UK) and a quartz cell with a 30-mL capacity and a 10-cm light path (for TPH concentration range from 0.5 mg L<sup>-1</sup> to 50 mg L<sup>-1</sup>) were used.

GC-FID analyses were performed using a Chrom-pack CP 9000 gas chromatograph (Apeldoorn, the Netherlands) with an FID detector using splitless injection. A WCOT Fused Silica, stationary phase: CP-SIL-8 CB (25 m × 0.25 mm i.d. with 0.4-µm film thickness) column was used. Nitrogen was used as carrier

gas and hydrogen and oxygen were used as FID gases. Maestro software was used for data acquisition and processing. Volumes of 1 µL were injected using a 10-µL microsyringe (Hamilton, IL, USA).

Determination of the organic matter content was performed with a Tecator<sup>TM</sup> Digestion System (Hillerød, Denmark) and water content was determined with a Lenton Furnaces oven (London, UK).

The wavenumbers used in the IR scans ranged from 3200 cm<sup>-1</sup> to 2700 cm<sup>-1</sup>, but absorbance was measured at the maximum peak of 2930 cm<sup>-1</sup> (subtracting the baseline). Calibration curves were constructed using six standard solutions with concentrations ranging from 4.91 mg L<sup>-1</sup> to 39.78 mg L<sup>-1</sup>. To reduce the detection and quantification limits of the GC-FID method, a pre-concentration step was included in the procedure where 10 mL of the extract was transferred into a vial and evaporated to dryness with a gentle stream of nitrogen and recovered with 1 mL of pentane. The temperature of the oven was programmed with an initial temperature of 40 °C (for 2 min) and a temperature rise of 6 °C min<sup>-1</sup> up to 290 °C. Detector and injector temperatures were set at 325 °C and 285 °C, respectively. Calibration curves for GC-FID were based on measurements of nine standard solutions with concentrations in the range from 500 mg L<sup>-1</sup> to 4000 mg L<sup>-1</sup>.

### *Samples and their treatment*

In total, fifteen samples were collected (three from five different sites: a farm, road, beach, commercial gas station, and vicinity of Portuguese oil refinery) in the north of Portugal. These groups of three samples were collected in distinct localities sufficiently distant to avoid soil similarities (minimum distance between sampling sites of the same type was 1.2 km). The five different types of locations chosen to study aimed at the collection of samples from sites that were presumably uncontaminated (farm and beach) and probably contaminated (roads, commercial gas stations, and vicinity of oil refinery). Approximately 1 kg of a sample was collected at each sampling point from the upper layer of soil of 0–20 cm using a spade. All samples

were thoroughly mixed to ensure homogeneity and, after air-drying and sieving through a 2-mm sieve, were stored at 4 °C (USEPA, 1996c).

For the extraction, approximately 3 g of soil was used and thoroughly mixed with 150 mL of extraction solvent and extracted over 4 h. The extraction was performed in triplicate in 1,1,2-trichloro-1,2,2-trifluoroethane for IR and pentane for GC-FID analyses, respectively (Current & Tilotta, 1997). After the extraction, 0.3 g of silica gel was added to adsorb the polar material, such as vegetable oils and animal fats. The USEPA method 8440 (USEPA, 1996c) regards all “oil and grease” materials that are not eliminated by silica gel adsorption as “petroleum hydrocarbons”. The extracts were filtered through Whatman GF/C filters (UK) using a DINKO D-95 vacuum pump (Barcelona, Spain). Sodium sulphate was added to the sample during the extraction procedure and in the filtration process to eliminate residual water. The extracts thus obtained were analysed by IR and GC-FID. Other procedures are described in the literature that use different solvents, such as tetrachloroethylene (Dumitran et al., 2009) or hexane (Rauckyte et al., 2010), or sonication methods to enhance extraction (Shin & Kwon, 2000; Miclean et al., 2010).

### *Recovery studies*

Recovery studies were performed using soils with different physical-chemical properties to verify whether the TPH content could be extracted from several types of soil. Hence, two soils samples, both from the north of Portugal, were collected: soil A (collected on a farm) and soil B (collected on a beach). After a preliminary analysis, it was observed that both soils did not contain detectable amounts of TPH.

These samples were fortified with reference oil and diesel standards for IR and GC-FID analyses, respectively at three levels: (I) 5000 mg kg<sup>-1</sup>, (II) 1000 mg kg<sup>-1</sup>, and (III) 500 mg kg<sup>-1</sup>. Pure 1,1,2-trichloro-1,2,2-trifluoroethane or pentane was added to both soils and samples were allowed to stand for 30 min before extraction, in order to obtain blanks. For fortification level I, and using IR, an aliquot of the extract (1 mL) was transferred into a 10-mL volumetric flask and diluted with 1,1,2-trichloro-1,2,2-trifluoroethane (final TPH concentration of 10 mg L<sup>-1</sup>). Level II and III samples could be analysed directly, because the final concentration was within the linear range of the calibration curve. For the GC analysis, an aliquot of the extract (10 mL) was transferred into a vial and evaporated to dryness with a gentle stream of nitrogen and re-dissolved with 1000 µL, 200 µL, and 100 µL of pentane for fortification levels I, II, and III, respectively (final TPH concentration of 1000 mg L<sup>-1</sup> for all fortification levels). A vortex mixer was used for homogenisation. The recovery was calculated by determining the percentage

Table 1. Analytical characteristics of analysed soils ( $n = 3$ )

Sample		Sample characteristics ( $\pm$ RSD <sup>a</sup> )			
ID	Sampling site	Density g mL <sup>-1</sup>	pH	Water content %	Organic matter content %
1	Farm (soil A)	0.7 $\pm$ 2.3	7.2 $\pm$ 1.5	15.6 $\pm$ 0.7	8.6 $\pm$ 1.1
2		0.7 $\pm$ 2.9	7.5 $\pm$ 1.4	12.2 $\pm$ 1.5	8.2 $\pm$ 1.9
3		0.6 $\pm$ 2.5	7.5 $\pm$ 1.6	16.8 $\pm$ 0.5	8.5 $\pm$ 0.9
4	Beach (soil B)	1.1 $\pm$ 3.3	7.3 $\pm$ 0.6	1.0 $\pm$ 3.0	1.1 $\pm$ 1.1
5		1.2 $\pm$ 2.7	7.6 $\pm$ 0.9	0.9 $\pm$ 4.8	0.9 $\pm$ 2.1
6		1.6 $\pm$ 1.1	7.6 $\pm$ 1.4	0.1 $\pm$ 3.2	1.3 $\pm$ 2.8
7	Road	1.6 $\pm$ 1.9	7.8 $\pm$ 1.1	0.1 $\pm$ 4.6	1.0 $\pm$ 1.6
8		1.2 $\pm$ 1.5	7.1 $\pm$ 1.8	1.0 $\pm$ 3.1	1.0 $\pm$ 3.3
9		1.6 $\pm$ 1.0	7.4 $\pm$ 1.1	0.0 $\pm$ 3.5	1.1 $\pm$ 0.9
10	Gas stations	1.0 $\pm$ 1.2	7.2 $\pm$ 1.6	2.4 $\pm$ 3.2	3.3 $\pm$ 2.8
11		1.2 $\pm$ 3.9	7.8 $\pm$ 2.3	1.3 $\pm$ 2.4	4.0 $\pm$ 2.8
12		1.0 $\pm$ 2.1	7.6 $\pm$ 1.0	2.1 $\pm$ 2.7	3.1 $\pm$ 2.4
13	Vicinity of oil refinery	0.8 $\pm$ 1.1	7.0 $\pm$ 1.2	3.7 $\pm$ 1.7	3.0 $\pm$ 2.5
14		0.8 $\pm$ 1.6	6.6 $\pm$ 1.7	3.0 $\pm$ 2.0	3.1 $\pm$ 1.8
15		1.4 $\pm$ 2.4	6.8 $\pm$ 1.0	0.2 $\pm$ 2.4	2.1 $\pm$ 2.7

a) Relative standard deviation.

of the amount of TPH added to the soil, quantified in the soil by both analytical methods.

The matrix effect was also evaluated analysing the equations of the calibration curves obtained using TPH standards prepared in solvent and in extract

solutions of soil A and B.

## Results and discussion

### Samples characterisation

Macro parameters (pH, density, water and organic matter content) for the fifteen soil samples were de-

termined (Hesse, 1972) and are shown in Table 1.

### Interferences

An IR analysis is always susceptible to interferences, so the results should be interpreted accordingly. If the organic matter is not fully removed in the silica gel clean-up, its presence may cause a positive error in the analysis. In soil A (high organic matter content) a strong absorbance was observed between 2700 cm<sup>-1</sup> and 3000 cm<sup>-1</sup>, in contrast to soil B (low organic matter content) where no absorbance was found (Fig. 1a). These interferences were not observed in the GC-FID analysis using soil A or soil B. Matrix effects were originally discussed by Tang and Kerbale (1993) and can lead to a significant increase or decrease in the response of an analyte in a sample compared with a pure standard solution. Matrix effects are attributed to interfering substances which co-extract with the analyte of interest and can be a cause of significant error

Table 2. Calibration data and assessment of matrix effect

	Determination	Calibration curve
Solvent	IR	$y = 1.13 \times 10^{-2}x + 3.87 \times 10^{-2}$
	GC-method A	$y = 2.48 \times 10^4x - 5.90 \times 10^6$
	GC-method B	$y = 5.08 \times 10^3x - 7.21 \times 10^4$
	GC-method C	$y = 3.08 \times 10^3x - 7.70 \times 10^4$
Soil A	IR	$y = 1.49 \times 10^{-1}x + 2.07$
	GC-method A	$y = 2.48 \times 10^4x - 5.90 \times 10^6$
	GC-method B	$y = 5.13 \times 10^3x - 1.44 \times 10^5$
	GC-method C	$y = 3.08 \times 10^3x - 5.52 \times 10^4$
Soil B	IR	$y = 1.13 \times 10^{-2}x + 4.90 \times 10^{-2}$
	GC-method A	$y = 2.47 \times 10^4x - 4.77 \times 10^6$
	GC-method B	$y = 5.07 \times 10^3x - 7.06 \times 10^4$
	GC-method C	$y = 3.09 \times 10^3x - 8.93 \times 10^4$

in the accuracy and precision of a method. Therefore, the evaluation of matrix effects is required as a part of quantitative method development (Annesley, 2003). Standard addition can be applied to several analytical methods and is used instead of the calibration curve to resolve the matrix effect (Harris, 2003). The standard addition method was used to determine TPH in all soil samples using IR or GC-FID. The results of the calibration curves (in solvent and in soil A and B extracts) are presented in Table 2.

From the similar slopes obtained in the GC-FID analyses, independently of the integration method used, it may be concluded that the soil matrix does not have an observable effect on the TPH analysis. On the

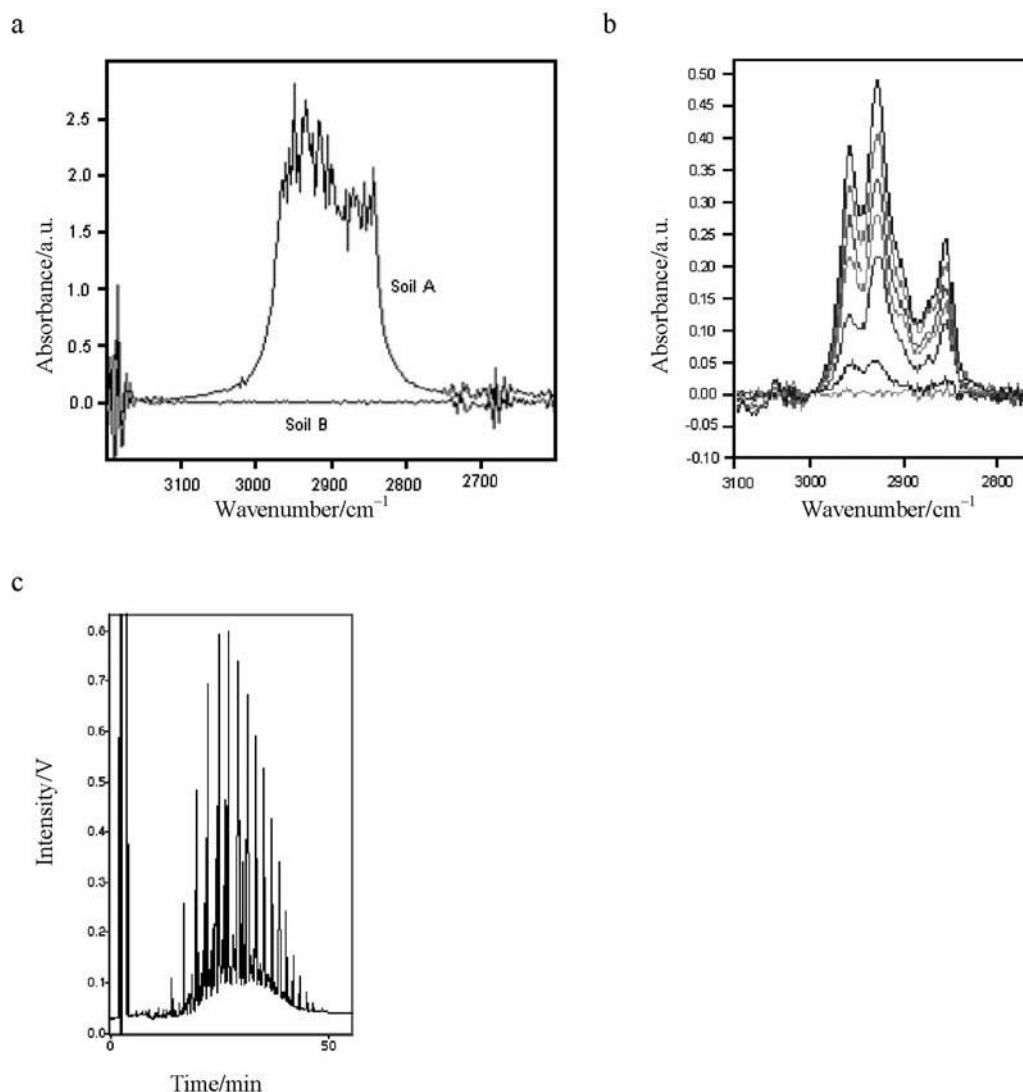


Fig. 1. Overlapped IR spectra of soil samples A and B (a), overlapped IR spectra of soil B and standard additions (concentrations of 4.91 mg L<sup>-1</sup>, 16.20 mg L<sup>-1</sup>, 21.25 mg L<sup>-1</sup>, 27.49 mg L<sup>-1</sup>, 33.84 mg L<sup>-1</sup>, and 39.78 mg L<sup>-1</sup>) (b), GC-FID chromatogram of standard solution (4000 mg L<sup>-1</sup>) in soil B (c).

other hand, a significant matrix effect was observed in soil A using IR method, resulting in the higher slope of the respective calibration curve. These results for soils with lower and higher organic matter justify the use of the standard addition method for all the samples analysed in order to reduce the matrix effects.

#### *Linearity, detection, and quantification limits of infrared and chromatographic methods*

Fig. 1b shows the spectra obtained in the analysis of the six standard solutions ranging from 4.91 mg L<sup>-1</sup> to 39.78 mg L<sup>-1</sup>. A linear response was obtained with a correlation coefficient of 0.9999. Under these conditions, the detection (LOD) and quantification limits (LOQ) were 2.62 mg kg<sup>-1</sup> (mg of TPH per kg of soil) and 8.73 mg kg<sup>-1</sup>, respectively. LOD and LOQ were calculated by multiplying the standard deviations of

the obtained linear regressions by 3 and 10, respectively, and dividing both by the slope of the respective linear regression equation, as described in Miller and Miller (2000). These results show that IR can be used for monitoring purposes.

A typical GC-FID chromatogram of a standard solution is shown in Fig. 1c. Integration of the peaks of the chromatograms was performed using three different methods (Fig. 2). In method A, denoted as “base-line to baseline”, the area considered represents the entire area of the chromatogram within the retention time-range for the fuel type, including the unresolved complex mixture. For the concentration range from 500 mg L<sup>-1</sup> to 4000 mg L<sup>-1</sup> (Fig. 2a), a linear response was obtained with a correlation coefficient of 0.9999. The total area was integrated from 14.1 min to 51.0 min (referring to decane and octacosane peaks, respectively). The LOD and LOQ were

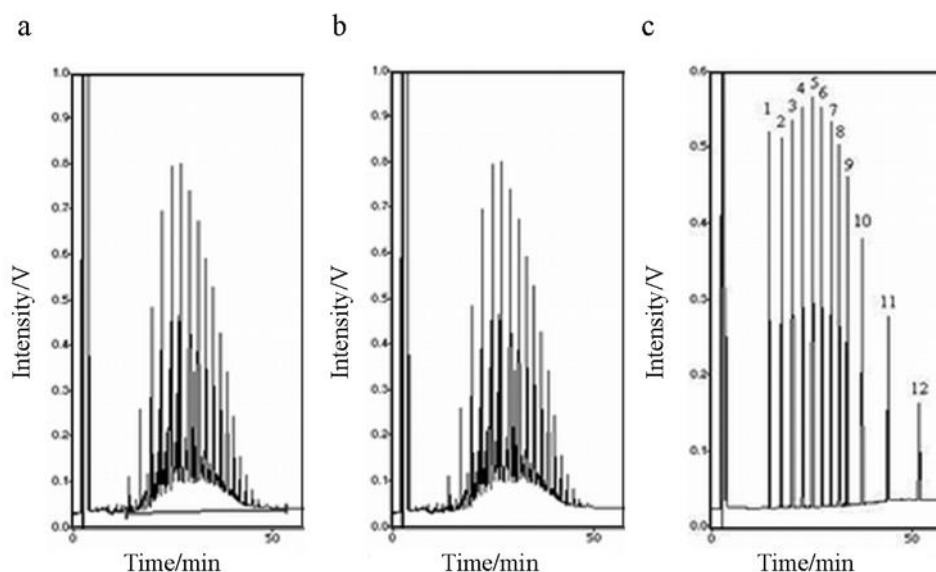


Fig. 2. GC-FID integration methods: “baseline to baseline” (a), “peak to peak” (b), and addition of ASTM standard solution (c). ASTM standard solution components: decane (1), undecane (2), dodecane (3), tridecane (4), tetradecane (5), pentadecane (6), hexadecane (7), heptadecane (8), octadecane (9), eicosane (10), tetracosane (11), and octacosane (12).

Table 3. TPHs recoveries (mean  $\pm$  relative standard deviation,  $n = 3$ ) from homogenised soil sample type A and B, at three fortification levels (I, II, and III)

method	Soil	Recovery/% ( $\pm$ RSD)				
		Fortification level mg kg <sup>-1</sup>	IR	GC-FID integration		
				A	B	C
A	I	5000	96 $\pm$ 1	98 $\pm$ 2	99 $\pm$ 2	98 $\pm$ 1
	II	1000	95 $\pm$ 1	98 $\pm$ 2	98 $\pm$ 1	98 $\pm$ 1
	III	500	94 $\pm$ 3	98 $\pm$ 2	98 $\pm$ 1	98 $\pm$ 2
B	I	5000	98 $\pm$ 1	98 $\pm$ 2	98 $\pm$ 2	98 $\pm$ 2
	II	1000	98 $\pm$ 2	98 $\pm$ 2	98 $\pm$ 2	98 $\pm$ 3
	III	500	98 $\pm$ 2	98 $\pm$ 1	97 $\pm$ 2	98 $\pm$ 2

127.07 mg kg<sup>-1</sup> and 423.57 mg kg<sup>-1</sup>, respectively. Using method B, denoted as “peak to peak”, only the twenty-seven most representative peaks in the chromatograms (Fig. 2b) were considered and integrated. In the range from 500 mg L<sup>-1</sup> to 4000 mg L<sup>-1</sup>, a linear response with a correlation coefficient of 0.9999 was obtained. The LOD and LOQ were 96.16 mg kg<sup>-1</sup> and 320.52 mg kg<sup>-1</sup>, respectively. The last integrated peak had a retention time of 51.0 min. Finally, in method C, the integration considered the retention times of the compounds included in the ASTM D5307 Crude oil quantitative STD analytical standard. Using the same conditions, an ASTM D5307 Crude oil quantitative analytical standard with a concentration of 960 mg L<sup>-1</sup> was injected. The mixture consisted of sixteen hydrocarbons, all of 6.25 mass %. The ASTM standard solution was injected in order to obtain the retention times for each hydrocarbon; then, diesel standard solutions (concentration range from

500 mg L<sup>-1</sup> to 4000 mg L<sup>-1</sup>) were injected and twelve peaks with the same retention time as the peaks of ASTM D5307 (Fig. 2c) were integrated. The last integrated peak had a retention time of 51.0 min. A linear response was obtained with a correlation coefficient of 0.9999. The LOD and LOQ were 118.54 mg kg<sup>-1</sup> and 395.13 mg kg<sup>-1</sup>, respectively.

Using GC-FID, methods A and B presented the lowest and highest LOD, respectively. IR provided a much lower LOQ than GC-FID but both methods enabled the quantification of lower amounts of TPH than the established alert and intervention values (Hesse, 1972).

#### Fortification levels

The extraction efficiency was consistent across the whole fortification range and for both soils (with different organic matter contents). No significant vari-

Table 4. Certified and measured concentrations of TPH in the ASTM D5307 (ASTM, 1997h) Crude oil quantitative standard ( $n = 3$ )

Component <i>a</i>	Purity Content		Retention time	Concentration/(mg L <sup>-1</sup> )			GC-FID (method C) <sup>e</sup>	
	RSD						Concentration ±SD	Recovery ±
	%	mass %	min	ASTM standard <sup>b</sup>	Extraction step <sup>c</sup>	Concentration step <sup>d</sup>	mg L <sup>-1</sup>	%
Decane	99.7	6.235	14.396	188.093	1.254	31.349	30.9 ±0.4	98.5 ±1.3
Undecane	99.2	6.235	17.296	187.149	1.248	31.192	30.9 ±0.3	98.9 ±0.9
Dodecane	99.6	6.235	20.044	187.904	1.253	31.317	30.6 ±0.5	97.7 ±1.6
Tridecane	99.3	6.235	22.632	187.338	1.249	31.223	30.7 ±0.1	98.4 ±0.4
Tetradecane	99.5	6.235	25.068	187.715	1.251	31.286	30.9 ±0.4	98.8 ±1.4
Pentadecane	99.8	6.235	27.372	188.281	1.255	31.380	31.0 ±0.3	98.7 ±0.9
Hexadecane	99.0	6.235	29.552	186.772	1.245	31.129	30.4 ±0.2	97.7 ±0.6
Heptadecane	99.0	6.235	31.620	186.772	1.245	31.129	30.9 ±0.2	99.1 ±0.6
Octadecane	98.7	6.235	33.584	186.206	1.241	31.034	30.3 ±0.0	97.7 ±0.1
Eicosane	99.0	6.241	37.240	186.952	1.246	31.159	30.6 ±0.4	98.3 ±1.2
Tetracosane	97.4	6.397	43.648	188.528	1.257	31.421	30.9 ±0.3	98.3 ±1.1
Octacosane	99.6	6.235	50.940	187.904	1.253	31.317	30.3 ±0.2	96.6 ±0.5
Dotriacontene <sup>f</sup>	99.3	6.235	—	187.338	1.249	31.223	—	—
Hexatriacontene <sup>f</sup>	99.6	6.235	—	187.904	1.253	31.317	—	—
Tetracontene <sup>f</sup>	99.2	6.235	—	187.149	1.248	31.192	—	—
Tetratetracontene <sup>f</sup>	99.7	6.235	—	188.093	1.254	31.349	—	—
For the 12 hydrocarbons	—	—	—	2249.614 <sup>g</sup>	14.997 <sup>g</sup>	374.936 <sup>g</sup>	368.3 <sup>g</sup>	98.2 ±0.7 <sup>h</sup>
For the 16 hydrocarbons	—	—	—	3000.098 <sup>g</sup>	20.001 <sup>g</sup>	500.016 <sup>g</sup>	—	—

a) See chromatogram in Fig. 2c; b) certified values, soil type B was contaminated with 1 mL of 3000 mg L<sup>-1</sup> ASTM standard solution; c) extraction of ASTM standard from 3 g of contaminated soil type B using 150 mL of pentane; d) value after pre-concentration (10 mL of the extract was evaporated with nitrogen and re-dissolved in 400 µL of pentane); e) values estimated experimentally; f) the last integrated peak was with retention time of 50.94 min; peaks not considered; g) total concentration measured for the twelve peaks; h) mean value for the twelve peaks.

ation in the results (Table 3) was observed and the recovery did not differ substantially at the lowest and the highest concentrations for the two types of soils. Three fortification levels were chosen in order to test the recovery values over a certain concentration range.

#### Analysis of ASTM D5307 Crude oil quantitative STD analytical standard

Validation of the extraction procedure for determination of TPH in soil samples was carried out by analysing a certified reference material. Standard ASTM D5307 solution (3000 mg L<sup>-1</sup>) was prepared in 1,1,2-trichloro-1,2,2-trifluoroethane and in pentane. Soil sample B (3 g) was contaminated with 1 mL of the standard ASTM solution and allowed to stand for 30 min before extraction. Using IR, determination of the concentration and recovery of individual hydrocarbons was not possible. The absorbance was measured and the concentration obtained was (19.6 ± 0.2) mg L<sup>-1</sup> ( $n = 3$ ) with the recovery of 97.8 % (RSD = 0.86 %,  $n = 3$ ). Using GC-FID, it was possible to calculate the concentration and recovery of each hydrocarbon present in the certified reference material. A pre-concentration step had to be performed (twenty-five times). Concentration and recoveries for each hydrocarbon are presented in Table 4.

The ASTM standard was successfully extracted from the soil sample with good recoveries in IR and GC-FID analyses. Referring to the similar slopes of the calibration curves obtained with soils A and B, the values of which are presented in Table 2, it can be deduced that if soil A were used, similar recoveries could have been achieved within the range of TPH concentrations studied.

#### Source of spilled oil

Each crude oil or petroleum product has its unique chemical “fingerprint”, providing a basis for identifying the source(s) of the spilled oil. Method 8440 cannot be applied to the analysis of petrol and other volatile petroleum fractions, because these fractions evaporate during sample preparation (USEPA, 1996c). To identify the specific fuel present in the soil samples analysed: a) diesel (1000 mg L<sup>-1</sup>) and b) petrol (1000 mg L<sup>-1</sup>) fuels were injected into a chromatograph with FID. The fuel chromatograms are presented in Fig. 3.

The chromatograms obtained for both samples are very specific and enabled the identification of the fuel in a specific sample. Therefore, all soil samples were analysed first by GC-FID and only the samples contaminated with diesel fuel were analysed by IR.

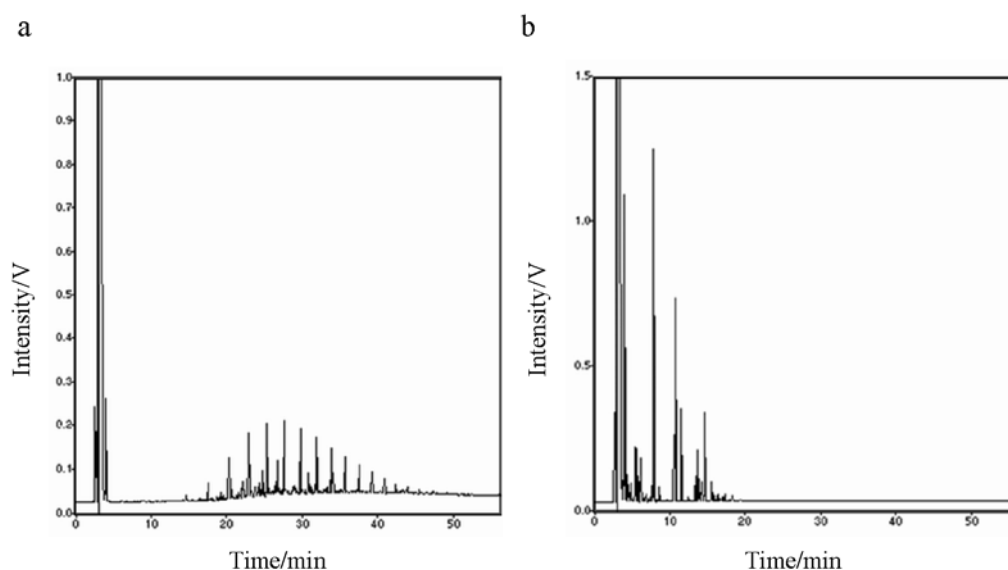


Fig. 3. GC-FID chromatograms of 1000 mg L<sup>-1</sup> diesel (a) and 1000 mg L<sup>-1</sup> petrol (b) fuels.

Table 5. Concentration of TPH in samples analysed (*n* = 3)

Sampling site	TPH concentration/(mg kg <sup>-1</sup> ) (± SD <sup>a</sup> )			
	IR	GC-FID integration		
		method A	method B	method C
Farm (soil A)	n.d.	n.d.	n.d.	n.d.
	n.d.	n.d.	n.d.	n.d.
	n.d.	n.d.	n.d.	n.d.
Beach (soil B)	n.d.	n.d.	n.d.	n.d.
	n.d.	n.d.	n.d.	n.d.
	n.d.	n.d.	n.d.	n.d.
Road	45 ± 2 <sup>b</sup>	< LOQ <sup>c</sup>	< LOQ <sup>c</sup>	< LOQ <sup>c</sup>
	64 ± 2 <sup>b</sup>	< LOQ <sup>c</sup>	< LOQ <sup>c</sup>	<
	LOQ <sup>c</sup> 55 ± 4 <sup>b</sup>	< LOQ <sup>c</sup>	< LOQ <sup>c</sup>	<
	LOQ <sup>c</sup>			
Gas stations	532 ± 25 <sup>d</sup>	561 ± 13	561 ± 30	567 ± 37
	649 ± 20 <sup>d</sup>	640 ± 11	628 ± 34	639 ± 10
	620 ± 21 <sup>d</sup>	650 ± 19	632 ± 19	608 ± 21
Refinery neighbourhood	8640 ± 149 <sup>e</sup>	8875 ± 152 <sup>f</sup>	8840 ± 209 <sup>f</sup>	9230 ± 322 <sup>f</sup>
	8029 ± 183 <sup>e</sup>	8326 ± 239 <sup>f</sup>	7973 ± 255 <sup>f</sup>	8235 ± 291 <sup>f</sup>
	3423 ± 213 <sup>e</sup>	3525 ± 309 <sup>f</sup>	3505 ± 225 <sup>f</sup>	3495 ± 253 <sup>f</sup>

a) SD – standard deviation; b) two times sample dilution (25 mL of extract in a 50 mL volumetric flask diluted with 1,1,2-trichloro- 1,2,2-trifluoroethane to the volume); c) fifty times sample pre-concentration (10 mL of extract evaporated to dryness with nitrogen and re-dissolved with 200 µL of pentane); d) twenty-five times sample dilution (2 mL of extract in a 50 mL volumetric flask diluted with 1,1,2-trichloro-1,2,2-trifluoroethane to the volume); e) two hundred and fifty times sample dilution (200 µL of extract in a 50 mL volumetric flask diluted with 1,1,2-trichloro-1,2,2-trifluoroethane to the volume); f) five times sample dilution (1 mL of extract in a 5 mL volumetric flask diluted with pentane to the volume).

#### Application to soil samples

collected near to a road

The results obtained for each soil sample are pre-sented in Table 5. IR and GC-FID determinations (in-tegration methods A, B, and C) showed similar re- sults. As an example, Fig. 4 presents the spectrum ob- tained by IR analysis of a soil



(sample 9) and a chromatogram obtained by GC-FID analysis of a soil collected in the vicinity of a refinery (sample 14).

In accordance with Dutch legislation (VROM, 1987), there are three limit values of TPH mass per mass of soil: reference (S,  $10 \text{ mg kg}^{-1}$ ), intervention (I,  $1000 \text{ mg kg}^{-1}$ ), and alert (T,  $505 \text{ mg kg}^{-1}$ ). The S

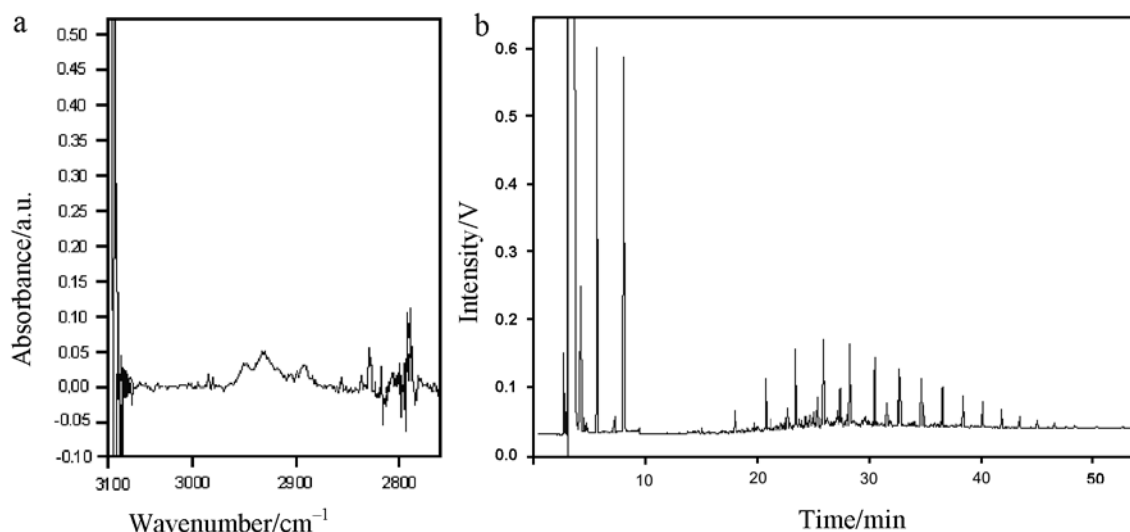


Fig. 4. Representative IR spectrum obtained for soil collected near to a road (sample 9) (a) and GC-FID chromatogram obtained for soil collected in the vicinity of an oil refinery (sample 14) (b).

value indicates the level at which the soil and ground-water are considered “clean”. The I value indicates the level above which it becomes a risk to human health and to the environment. The higher values (average) in 25 m<sup>3</sup> of soil or 100 m<sup>3</sup> of groundwater indicate that T value is the average value between S and I.

The TPH concentration in the samples from gas stations were higher than the Dutch T alert value and in the samples collected in the vicinity of a refinery TPH concentrations were above the Dutch I intervention value. The results in Table 5 also indicate that the soils collected from a beach and in a farm present no detectable levels of contamination, confirming classification of presumed uncontaminated soils. The soil collected near to a road showed levels of TPH which did not attain the Dutch alert value, indicating that the soil, classified as potentially contaminated, was uncontaminated but required future monitoring. Finally, the soils collected within gas stations and in the vicinity of an oil refinery confirmed the potentially contaminated status accorded and required remediation action.

### Conclusions

The present work demonstrates that IR and GC-FID can be considered suitable for detection and quantification of TPH in soil samples, considering different levels of contamination (ranging from not detectable levels, in soils collected from a farm and a beach, up to  $(9230 \pm 322)$  mg kg<sup>-1</sup> in soil collected from the vicinity of an oil refinery). However, utilisation of IR is not advisable for soils contaminated with petrol because of the volatilisation losses that occur in the analytical process.

The IR method presents limits of detection and quantification of 3 mg kg<sup>-1</sup> and 9 mg kg<sup>-1</sup>, respectively; the gas chromatography method present lim-

its of detection and quantification within the ranges of 96 mg kg<sup>-1</sup> to 127 mg kg<sup>-1</sup> and 321 mg kg<sup>-1</sup> to 424 mg kg<sup>-1</sup>, respectively, depending on the integration method used. Recovery experiments with soil with high organic matter content using the IR procedure provided satisfactory average recovery (around 94 %) and the respective standard deviation values which were comparable with those obtained by gas chromatography (higher than 97 %).

The volume of solvent used with the GC-FID method is lower than that used with the IR method, avoiding the use of hazardous solvent (1,1,2-trichloro- 1,2,2-trifluoroethane) and reducing cost per analysis. This volume reduction further decreases waste generation and analyst exposure. There are fewer interferences resulting from organic matter content in the GC-FID method and the analytical costs are lower than with the IR method, although the GC-FID is more time-consuming.

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